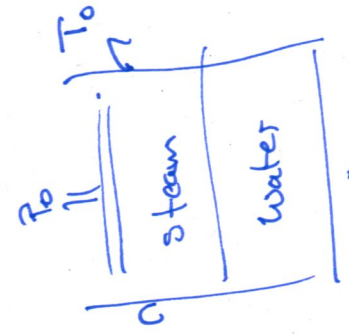
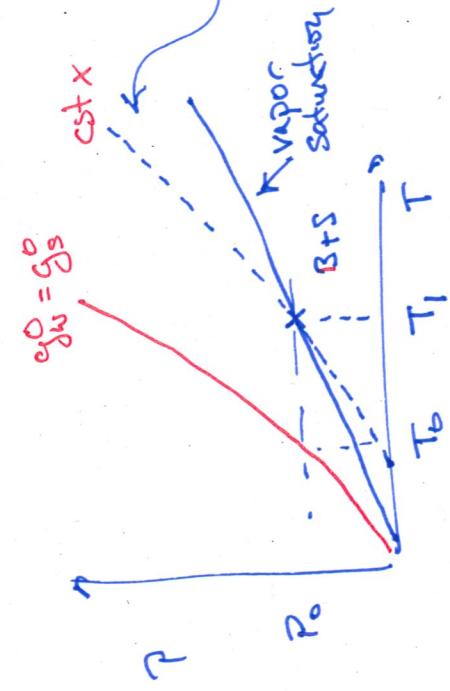
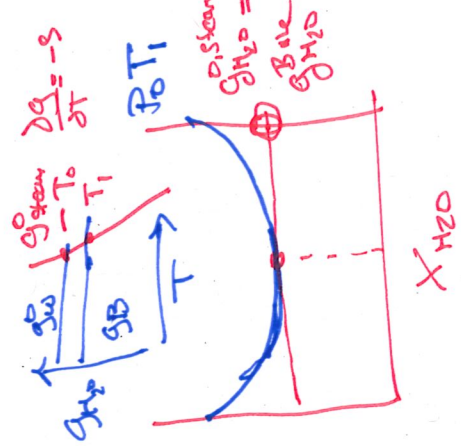
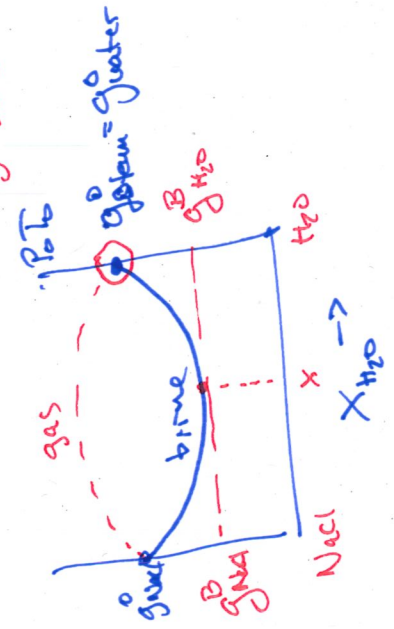


Thermobarometry → Problem 8.2

L 13.1 2021



why add salt?



$$\mu_{H_2O} = \frac{\partial G_{system}}{\partial N_{H_2O}} = G_{H_2O}^{steam} = G_{H_2O}^{water}$$

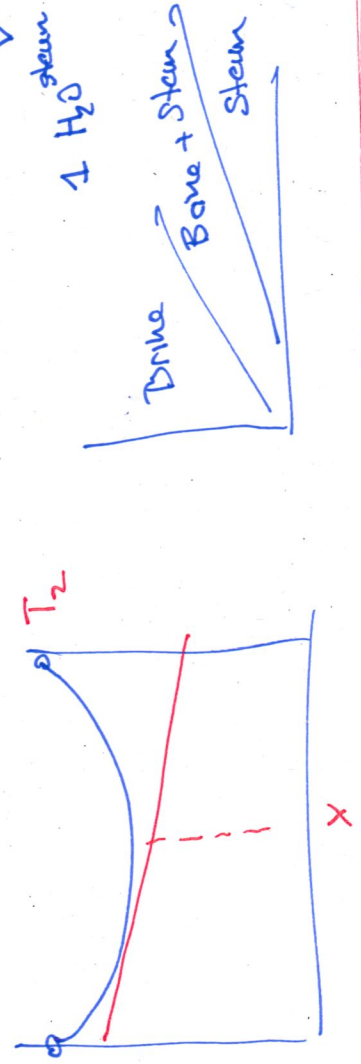
$$= \frac{\partial G}{\partial N_{H_2O}} = G_{H_2O}^0 + S(x) = G_{H_2O}^{brine}$$

$$\text{activity}$$

thermobarometric curve assumes X is fixed (observed) and $G_{H_2O}^{brine} = G_{H_2O}^{steam}$

necessary condition

1 H_2O steam = 1 H_2O water



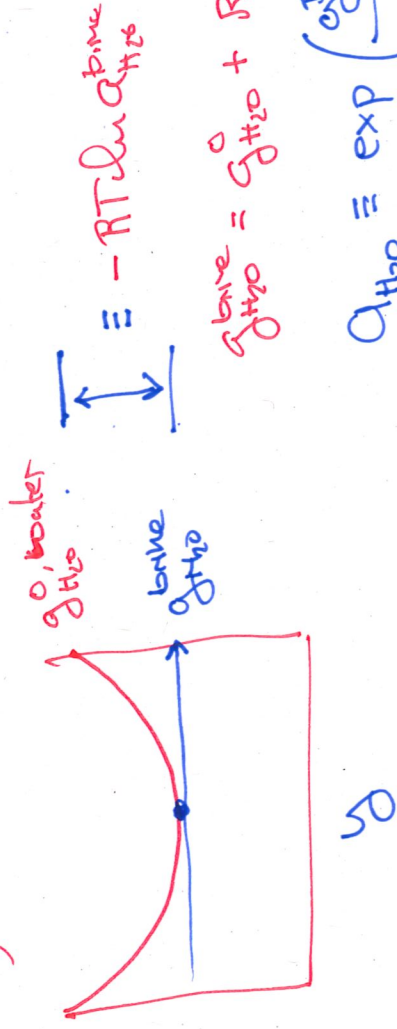
Generalization: the change in partial molar G 's must be zero for any stoichiometric reaction that can be written among the species/endmembers of an eq system

$$\Delta G = \sum \nu_i G_i \Rightarrow \Delta G = \sum \nu_i \mu_i \text{ at eq } G_i^j = \mu_i^*$$

$$\Delta G = \sum \nu_i \mu_i = \sum \nu_i \mu_i^*$$

$$\Delta G = \sum \nu_i \mu_i^* \Rightarrow \sum \nu_i \mu_i^* = \Delta G = 0$$

* assuming for simplicity, in general G_i^j can be written as a linear comb of μ

activity $\Rightarrow$ 

$$g_{H_2O}^{pure} = g_{H_2O}^0 + RT \ln a_{H_2O}$$

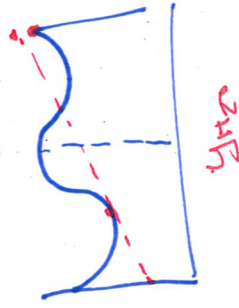
$$a_{H_2O} \equiv \exp \left(\frac{g_{H_2O}^{pure} - g_{H_2O}^0}{RT} \right)$$

1) If $g^{\text{ex}} = 0$ and $g^{\text{conf}} = -R \sum y_i \ln y_i$ (ie a molecular model)

then $G = y \Rightarrow$ hence the notion of "thermodynamic concentration".

2) in general $a \neq y$ but $a(y)$ such that $y \rightarrow 1 \rightarrow a \rightarrow 1$
TEST #1 $\Rightarrow$ 1st test $\Rightarrow$ for any activity formulation

3) For any stable composition of a solution $a(y) \leq 1$
 it is not required that $a_{H_2O} \rightarrow 0$
 when $y_{H_2O} \rightarrow 0$



Fugacity vs activity

activity $g_i = g_i^0(P,T) + RT \ln a_i$ $a_i = y_i$ ideal

fugacity $g_i = g_i^0(P,T) + RT \ln f_i$
 $= g_i^0(P,T) + \int_{P_r}^P V_i^{\text{vap}} dP \rightarrow RT \ln (P/P_r)$
 $\hat{g}_i = y_i P$ technically

$$g_i^0(P,T) = g_i^0(P,T) + \int V_i^{\text{vap}}$$

$V_i = RT/P \Leftarrow$ ideal gas

$$g_{\text{sol}} = g_{\text{mech}} + g^{\text{conf}}$$

$$\frac{f_{i,P}}{f_{i,P_r}} = y_i \frac{P}{P_r}$$

but at 1 bar $f_{i,P_r} = P_i$

geologically formulated solution models

$$g^{\text{sol}} = g^{\text{mech}} + g^{\text{conf}} + g^{\text{ex}}$$

$$\Rightarrow \text{irrationally } g^{\text{sol}} = \sum y_i g_i^{\text{sol}} \Rightarrow g_i = g_i^0 + RT \ln a_i$$

$$= \sum y_i (g_i^0 + RT \ln a_i)$$

$$= \sum y_i g_i^0 + \sum y_i RT \ln a_i$$

$$g^{\text{conf}} = +RT \sum y_i \ln a_i^{\text{ideal}} \leftarrow g^{\text{conf}}$$

$$g^{\text{ex}} = RT \sum y_i \ln \gamma_i$$

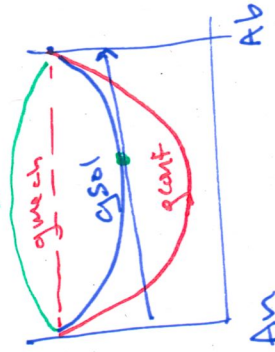
$$RT \left(\sum y_i (\ln a_i^{\text{ideal}} + \ln \gamma_i) \right)$$

γ_i the activity coefficient

getting g_i, a_i, f_i from g

$$g_i^{\text{sol}} = \frac{\partial g^{\text{sol}}}{\partial N_i} \neq \frac{\partial g}{\partial y_i}$$

only 2-1 independent y_i 's!!!



$g^{\text{sol}}(y_{\text{ab}})$

$$g_{\text{ab}}^{\text{PI}} = g^{\text{PI}}(y_{\text{ab}}) + \frac{\partial g^{\text{PI}}}{\partial y_{\text{ab}}} (1 - y_{\text{ab}})$$

$$g_{\text{An}}^{\text{PI}} = g^{\text{PI}}(y_{\text{ab}}) + \frac{\partial g^{\text{PI}}}{\partial y_{\text{ab}}} (0 - y_{\text{ab}})$$

preferable because of symmetry

$\rightarrow$ for $g^{\text{sol}}(y_i)$ ie $i \neq j$

$$g_i^{\text{sol}} = g^{\text{sol}}(y_i) - \sum_{j \neq i} y_j \frac{\partial g}{\partial y_j}$$

[[Test #2]] $\rightarrow a_i \neq f(g_i)$ [for simple solution models]



Back to Thermobarometry $\Rightarrow$ problem 8.2

Mg, Fe
 $\text{garnet} + \text{plagioclase} + \text{qtz} + \text{Kfs}$
 $\text{CaAl}_2\text{Si}_2\text{O}_8$
 $\text{all 4 phases exist in CaO-Al}_2\text{O}_3\text{-SiO}_2$ $\text{Kfs} = 3$ $\text{reaction} = 3+1$ phases
 Na, Ca
 $\text{Al} \Rightarrow \text{C} = 6 \Rightarrow \text{reaction} = 6+1$ phases

(GASP) $3\text{an} - \text{qtz} - 2\text{kfs} - \text{fs} = 0$ $\Delta G = 0$

necessary condition!

$$\begin{aligned}
 \Delta G &= \sum \nu_i \ddot{g}_i = \sum \nu_i (g_i^\circ + RT \ln a_i) \\
 &= \sum \nu_i g_i^\circ + \sum \nu_i RT \ln a_i \\
 &= \Delta G^\circ + \sum RT \ln a_i^{\nu_i} \\
 &= \Delta G^\circ + RT \ln (\prod a_i^{\nu_i}) \\
 &= \Delta G^\circ + RT \ln \left(\frac{a_{\text{an}}^3}{a_{\text{qtz}} a_{\text{kfs}}^2} \right)
 \end{aligned}$$

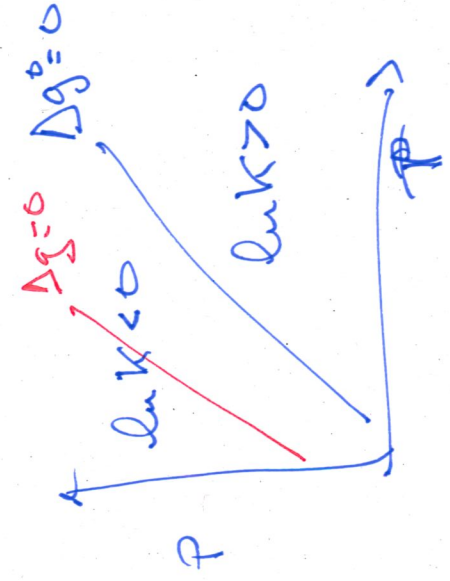
eq constant:

$$K \equiv \prod a_i^{\nu_i}$$

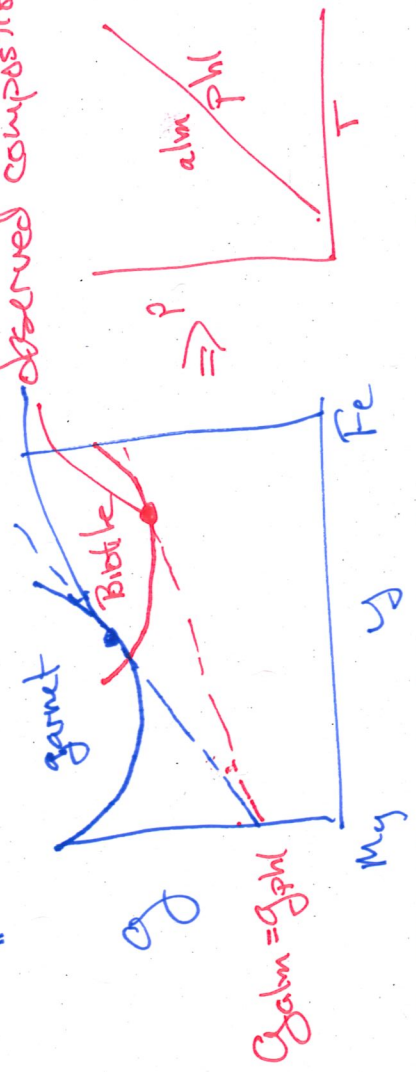
$K(P, T, \nu_i) \Rightarrow y_i$ observed.

Inverse method

- 1) plug in observed compositions compute $\Delta G(T) = 0 \Rightarrow$ gives "curve"
- 2) introduce 2nd constraint
- 3) always works $\Leftarrow$ why it's bad
- 3) empirical calibration $\Leftarrow$ why it's good



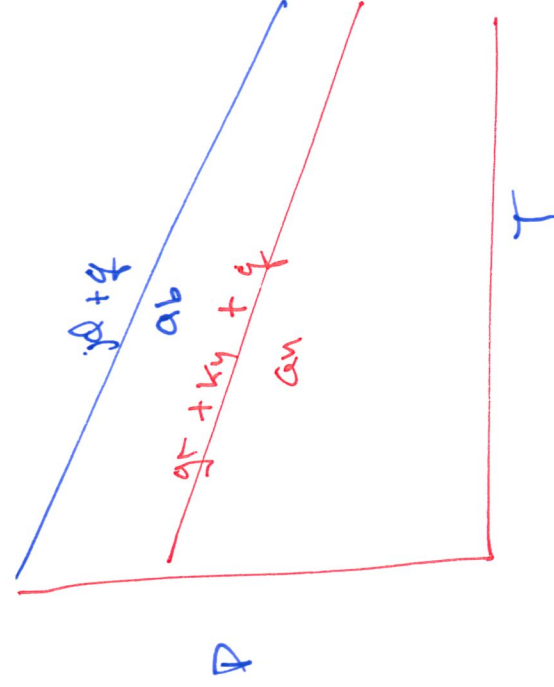
observed compositions



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$$+ C_p x \quad G + P + C_p x + Q + L$$

The Problem $\rightarrow$ necessary but not sufficient



$$a_n = g_r + k_y + q \quad n: P$$

$$a_b = j_d + q \quad n: P$$

uncertainty - non-equilibrium
- bad data

even if they do cross

- it only means the
phases could have
been - stable

Problem 8.2



$$g^t = g^t - y_{alm} y_{py} \left(\frac{dg^t}{dy_{py}} \right) - y_{alm} \left(\frac{dg^t}{dy_{alm}} \right)$$



Problem 8.4

- 1) $g_{ab}^i = f(y_{ab}^i)$, $g_{ab}^j = f_2(y)$
- 2) $T < T_c \rightarrow g_{ab}^{miss} = g_{ab}^{miss} = g_{ab}^{miss}$
- 3) $g_{ab}^{miss} = \text{subs}(y = y_1, g_{ab})$
 $g_{ab}^{miss} = \text{"}(y = y_1, g_{ab})$
- 4) $f_{\text{solve}}(g_{ab}^{miss} = g_{ab}^{miss}, g_{ab}^{miss} = g_{ab}^{miss}, g_{ab}^{miss} = g_{ab}^{miss})$