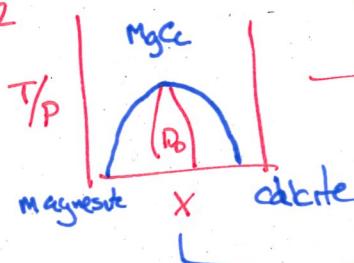


10 [vz] possible problem sets \Rightarrow 9 count
0, 1, 2, 4, 3, 4, 5, 6, 8a, 8b, 11, [9.1], [7]

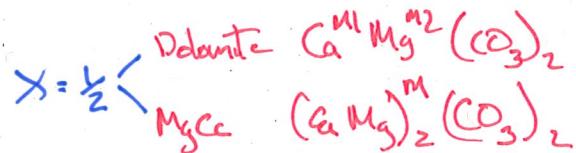
Problem 0.1 \rightarrow solvus \rightarrow Chp 8.1 (solvus can be calculated)

Problem 0.3, 0.4 \rightarrow Chp 6 (q) quantitatively w/script for problem q.1)

Problem 0.2



ergodic hypothesis does not allow variable order



Why?

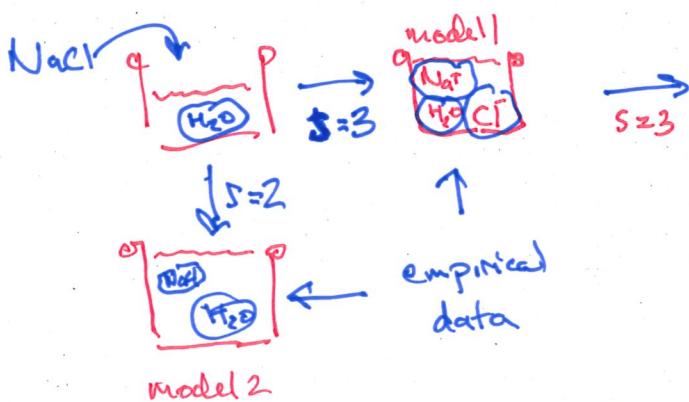
Do scmt sub] \rightarrow measured by G_f
MgCO₃ low high usually referred
high low to as "enthalpic
stabilization"

Speciation (aka order-disorder or compound formation) models. Components vs. Species

Water \rightarrow C = 1 \rightarrow H₂O, max C = 2 \rightarrow H₂, O₂ \rightarrow C \leq # of elements
if stoichiometric | if nonstoichiometric

physics \rightarrow t-species H₂O, H₂, O₂, OH⁻, H⁺, H₂O₂ ... there is no
thermodynamic restriction on species \rightarrow used in thermo
only to facilitate (simplify) empirical solution models

Two kinds of speciation models \rightarrow Primitive \rightarrow t = C endmembers
 \rightarrow microscopic speciation stoichiometrically prescribed (ergodic)
 \rightarrow nothing new (plagioclase) \rightarrow looks different for fluids
and melts: NaCl + H₂O \Rightarrow C = 2 (!)



y \rightarrow endmember fraction ($\Sigma = 1$)

z \rightarrow species fraction ($\Sigma = 1$)

n_{TOT} \rightarrow total number of mols of species

$$n_{TOT} = y_{H_2O} + 2y_{NaCl} \Rightarrow y_{H_2O} = 1 - y_{NaCl} = 1 + y_{NaCl}$$

Chapter 11.1 2022



Note correction (yesterday)
to Eq 11.11 $y = y'/\Sigma$

$$s=3 \text{ cont'd} \Rightarrow z_{Na^+}^* = \frac{n_{Na^+}}{n_{\text{TOT}}} = \frac{y_{\text{NaCl}}}{1+y_{\text{NaCl}}} [= z_{Cl^-}]$$

$$z_{H_2O} = \frac{n_{H_2O}}{n_{\text{TOT}}} = \frac{1-y_{\text{NaCl}}}{1+y_{\text{NaCl}}}$$

$$\begin{aligned} -\frac{s^{\text{conf}}}{R} &= z_{Na^+} \ln z_{Na^+} + z_{Cl^-} \ln z_{Cl^-} + z_{H_2O} \ln z_{H_2O} \\ &= 2 \frac{y_{\text{NaCl}}}{1+y_{\text{NaCl}}} \ln \left(\frac{y_{\text{NaCl}}}{1+y_{\text{NaCl}}} \right) + \frac{1-y_{\text{NaCl}}}{1+y_{\text{NaCl}}} \ln \left(\frac{1-y_{\text{NaCl}}}{1+y_{\text{NaCl}}} \right) \xrightarrow{y_{\text{NaCl}} \rightarrow 0} \\ &\quad \cancel{y_{\text{NaCl}}} \qquad \cancel{y_{\text{NaCl}}} \qquad \cancel{y_{\text{NaCl}}} \\ -\frac{s^{\text{conf}}}{R} &= y_{\text{NaCl}} \ln y_{\text{NaCl}}^2 = y_{\text{NaCl}} \ln (a_{\text{NaCl}}^{\text{ideal}}) \xrightarrow{a_{\text{NaCl}}^{\text{ideal}} = y_{\text{NaCl}}} \end{aligned}$$

intro chemistry

model 2 $s=2$

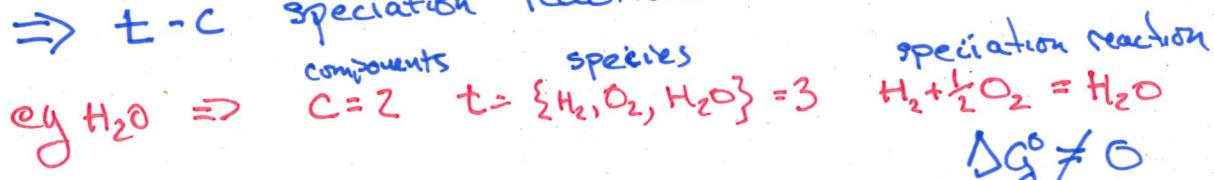
$$\begin{aligned} -\frac{s^{\text{conf}}}{R} &= y_{\text{NaCl}} \ln y_{\text{NaCl}} + y_{H_2O} \ln y_{H_2O} \xrightarrow{y_{\text{NaCl}} \rightarrow 0} \\ &= y_{\text{NaCl}} \ln a_{\text{NaCl}} \qquad a_{\text{NaCl}} = y_{\text{NaCl}} \end{aligned}$$

silicate melt models are generally of this form ($t=c$)

Non-ergodic speciation models (order-disorder, compound formation)

$\Rightarrow t > c$ end members (species)

$\Rightarrow t - c$ speciation reactions



$c = 1 \Rightarrow$ solution model \Rightarrow oxygen O [O₂, O₃, ...] & Thermodynamics

$t = 2 \Rightarrow$ O₂, O₃ species ← physics

$t - c = 1 \Rightarrow$ speciation reactions $\frac{3}{2}O_2 - \frac{2}{2}O_3 = O \quad \Delta\alpha = 3-2 = 1$

$$g^{\text{sol}} = \sum_{i=1}^c y_i g_i^\circ - T s_{\text{const}} + g^{\text{ex}} \quad \text{to for simplicity}$$

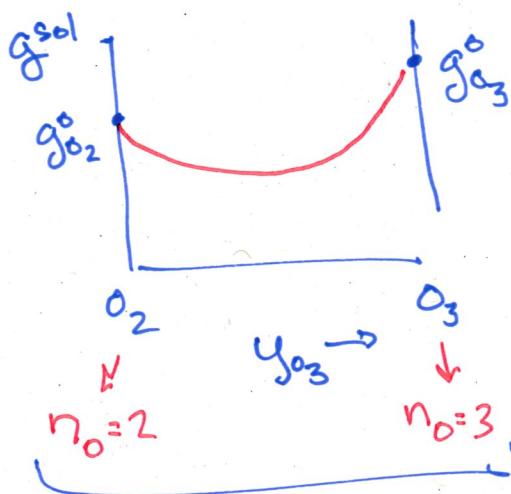
for homogeneous phase relations C of the

g_i° values may be set = 0 $\Rightarrow \sum_{i=1}^c y_i \Delta g_i^\circ$

$$= y_{O_3} \Delta g_{O_3}^\circ$$

$$g^{\text{sol}} = y_{O_3} \Delta g_{O_3}^\circ - RT(y_{O_3} \ln y_{O_3} + y_{O_2} \ln y_{O_2})$$

\Rightarrow eliminate $y_{O_2} (= 1 - y_{O_3}) \Rightarrow g(y_{O_3})$



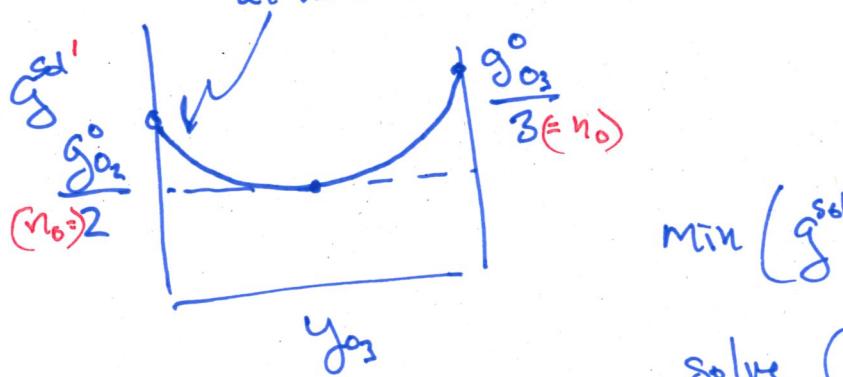
$g^{\text{sol}} \rightarrow$ TS g/mole-of-species

we need g/mole-of-atoms

For one atom $n_O = 2 + y_{O_3}$

$$g^{\text{sol}'} = \frac{g^{\text{sol}}}{n_O} = \frac{g^{\text{sol}}}{2 + y_{O_3}}$$

generalization in
Chp 11 exp 6-11

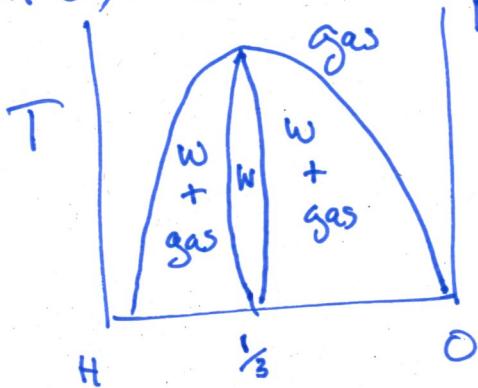


$$\min(g^{\text{sol}'}(y_{O_3})) \Rightarrow$$

$$\text{solve } (\text{d.f.}(g^{\text{sol}'}, y_{O_3}))$$

$c > 2 \quad t > c$ convergent ordering

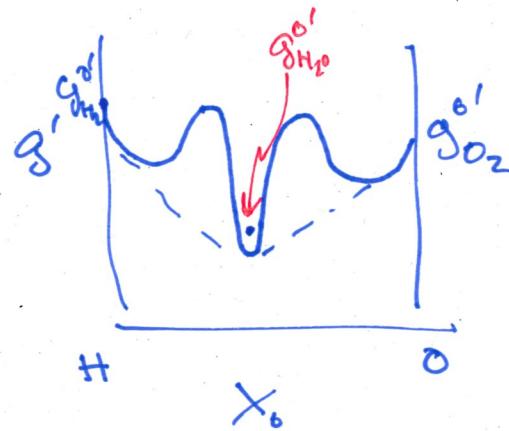
H-G, $c=2$



$P < P_{crit} \approx 212\text{ bar}$

$c=2$

$$t=3 = \left\{ \begin{array}{l} \text{H}_2 \\ \text{O}_2 \\ \text{H}_2\text{O} \end{array} \right\}$$

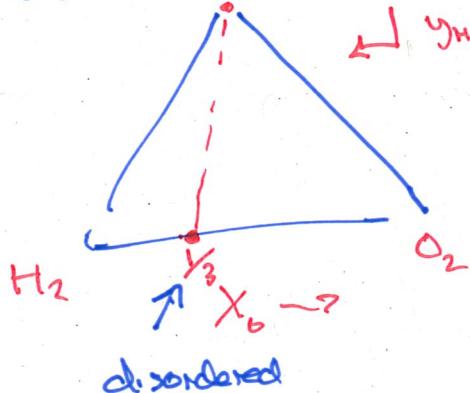


$X_0 \rightarrow$

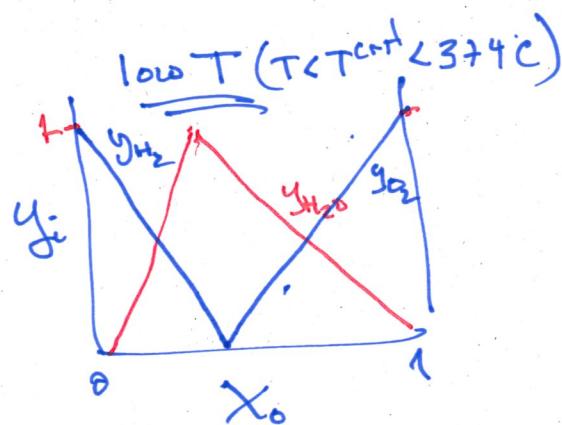
↳ Bulk composition

ordered $\Rightarrow \text{H}_2\text{O}$ Speciation composition

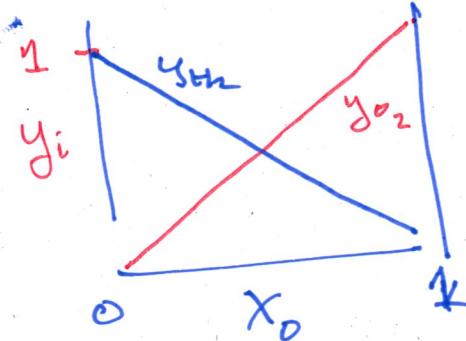
$$\downarrow y_{\text{H}_2\text{O}}, y_{\text{H}_2}, y_{\text{O}_2}$$



disordered



high $T \Rightarrow y_{\text{H}_2\text{O}} = 0$



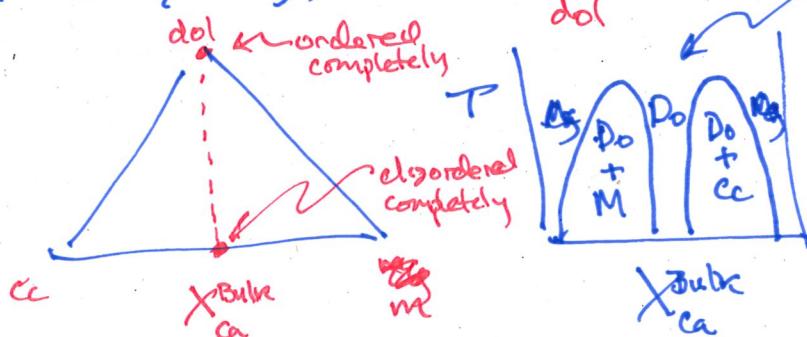
Solids do-cc-m (problem 11.1 omphacite jd-di-sm)

$c=2 \{ \text{CaCO}_3, \text{MgCO}_3 \}$

means there MUST be 2 crystallographically distinct sites for Ca/Mg

$t=3 \{ \overset{\text{cc}}{\text{CaCO}_3}, \overset{\text{m}}{\text{MgCO}_3}, \overset{\text{dol}}{\text{Ca}_5\text{Mg}_5(\text{CO}_3)_6} \}$

non-convergent (no transition to completely disordered phase)



→ we need

$$g_{\text{sol}}^{\text{sol}}(X_{\text{Ca}}, Y_{\text{Ca}})$$

Endmember site occupancies
and multiplicities

	M1	M2
cc	Ca	Ca
m	Mg	Mg
do	Mg	Ca
gi	y_2	y_2

1) formulate $g_{\text{sol}}(y)$

$$g^{\text{mech}} = y_{\text{cc}} g_{\text{cc}}^0 + y_m g_m^0 + y_{\text{do}} g_{\text{do}}^0 \Rightarrow c=2 \rightarrow s_b$$

For internal phase relations we may set $g_{\text{cc}}^0 = g_m^0 = 0$

and $g^{\text{mech}} = y_{\text{do}} g_{\text{do}}^0$ ($g_{\text{do}}^0 = N_g^0$ for the pure ordering rm)

$$g^{\text{conf}} = -RT \left\{ \frac{1}{2} \left[z_{\text{ca}}^{M1} \ln z_{\text{ca}}^{M1} + z_{\text{mg}}^{M1} \ln z_{\text{mg}}^{M1} \right] + \frac{1}{2} \left[z_{\text{ca}}^{M2} \ln z_{\text{ca}}^{M2} + z_{\text{mg}}^{M2} \ln z_{\text{mg}}^{M2} \right] \right\}$$

From site occupancy table $z_{\text{ca}}^{M1} = y_{\text{cc}}$ $z_{\text{mg}}^{M1} = 1 - y_{\text{cc}}$
 $z_{\text{mg}}^{M2} = y_m$ $z_{\text{ca}}^{M2} = 1 - y_m$

$g^{\text{ex}} = 0$ for simplicity, in general an excess function
as in normal solutions (and in problem 11.1)

2) convert to $g^{\text{sol}}(x_{\text{ca}}, y_{\text{do}})$

a) $x_{\text{ca}} = \frac{n_{\text{ca}}}{n_{\text{ca}} + n_{\text{mg}}} \quad n_{\text{ca}} = y_{\text{cc}} + \frac{1}{2} y_{\text{do}}$
 $n_{\text{mg}} = y_m + \frac{1}{2} y_{\text{do}}$
 $n_{\text{tot}} = y_{\text{cc}} + y_{\text{mg}} + y_{\text{do}} = 1$

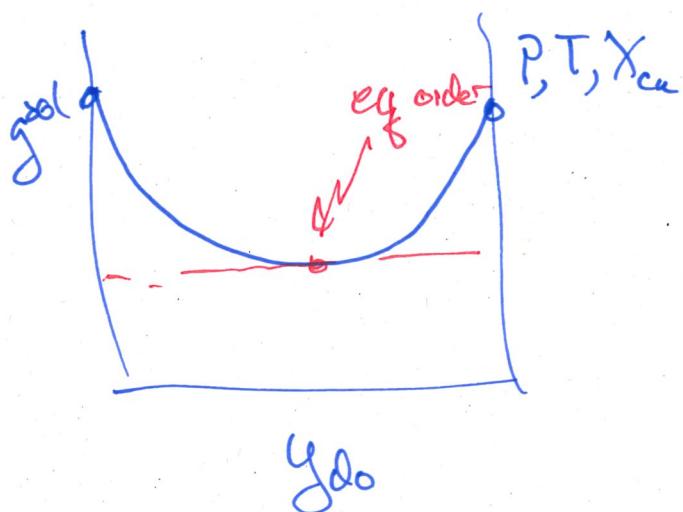
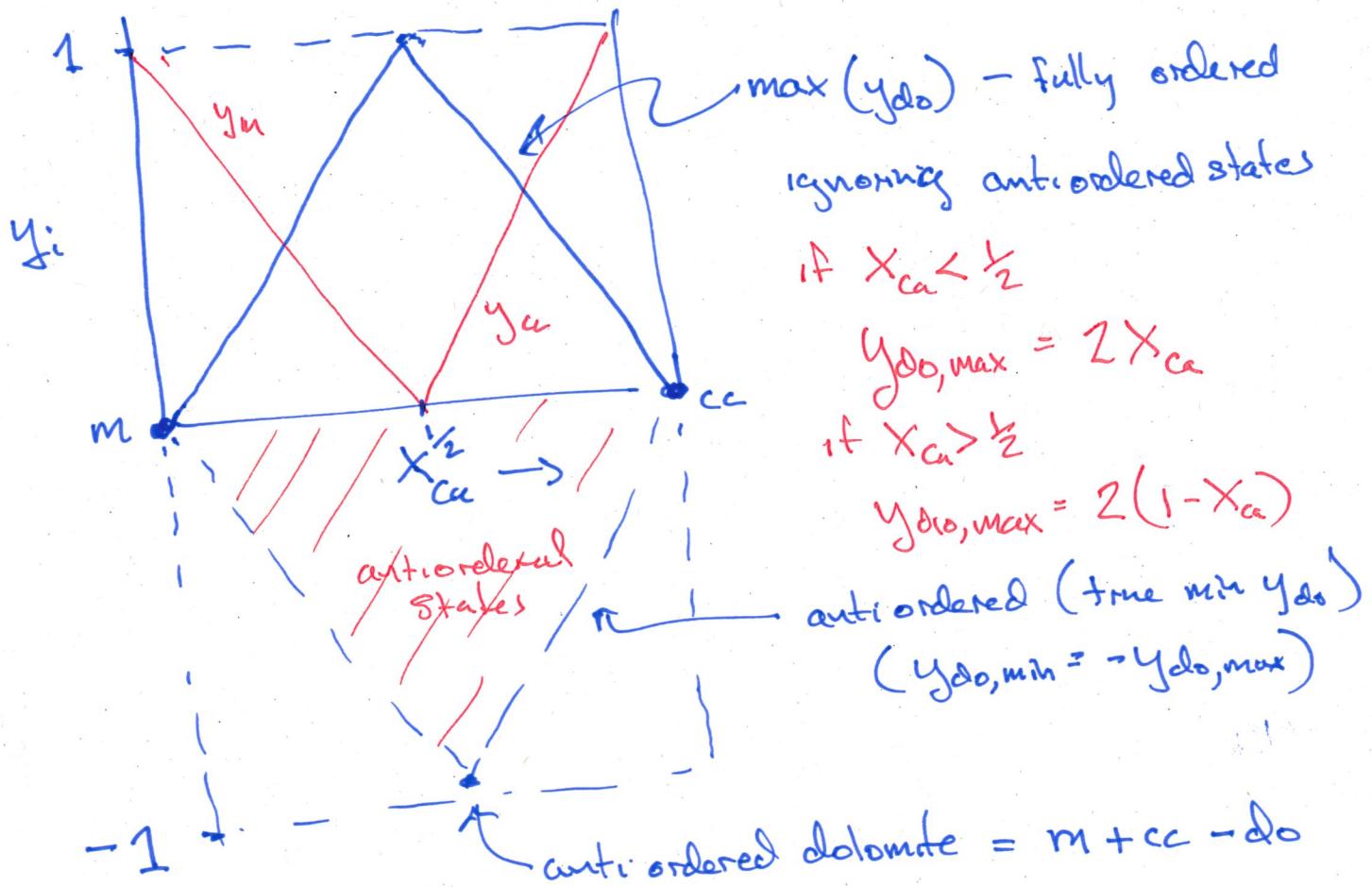
$$x_{\text{ca}} = y_{\text{cc}} + \frac{1}{2} y_{\text{do}}$$

$$g(x_{\text{ca}}, y_{\text{do}}, y_m) \Leftarrow \Rightarrow y_{\text{cc}} = x_{\text{ca}} - \frac{1}{2} y_{\text{do}}$$

b) use closure to eliminate $y_m \Rightarrow$

$$y_m = 1 - y_{cc} - y_{do} \Rightarrow y_{cc} = x_{ca} - \frac{1}{2} y_{do}$$

$$y_m = 1 - x_{ca} - \frac{1}{2} y_{do} \Rightarrow g(x_{ca}, y_{do})$$



$$\min(g_{sol}) \text{ at cst } P, T, X_{ca}$$

\Rightarrow

$$\text{solve } (\text{diff}(g, y_{do} = 0 \dots y_{do,\min}))$$

and x_{ca} or $y_{do,\min}$
given y_{do} ; y_{cc} and y_m
can be obtained by back
substitution

Order parameters

$$Q = [-1, 1]$$



usually expressed as the difference in site fractions
for some element, e.g. here (and in problem 11.1)

$$Q = z_{M_1}^{M_1} - z_{M_2}^{M_2} = (y_m + y_{d0}) - (y_m) = y_{d0}$$

Why bother?
