

isolated system $U(S, \psi_1, \dots, \psi_{k+2})$

$c = k+2 = \#$ of conservative properties, i.e. $U, \psi_1, \dots, \psi_{k+2}$
 real processes: $\delta S_{\text{un}} > 0$ stable system: $\delta S_{\text{un}} < 0$

system open with respect to $\psi_{c+1}, \dots, \psi_{k+2} \Rightarrow U + \sum_{c+1}^{k+2} \psi_{c+1} = 0$

$\Omega(\psi_1, \dots, \psi_c, \psi_{c+1}, \dots, \psi_{k+2}) =$ Legendre Transform $\Omega \equiv U - \sum_{c+1}^{k+2} \psi_{c+1}$

Can only be used to predict stability at constant $\psi_{c+1}, \dots, \psi_{k+2}$

Two cases:
 — only case of interest is $H(S, M_1, \dots, M_k, P)$

Adiabatic

$\Omega(S, \psi_1, \dots, \psi_c, \psi_{c+1}, \dots, \psi_{k+2})$

$c = k+2 = (\Omega, \psi_1, \dots, \psi_c)$

real processes $dS > 0, d\Omega = 0$, stability ...

Diathermal

$\Omega(\psi_1, \dots, \psi_c, T, \psi_{c+1}, \dots, \psi_{k+2})$

conservative properties $\psi_1, \dots, \psi_c$

real processes $d\Omega = -TdS_{\text{int}} < 0$

stability $d\Omega_{c+1, \dots, c_{k+2}}^T > 0$

isTP!

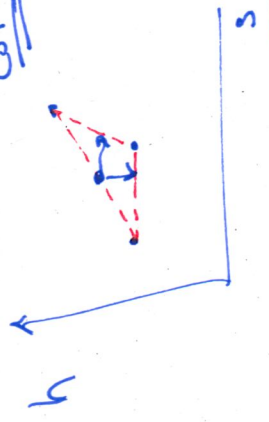
$c = \{H, N\}$

$\psi_{c+1} = -P$

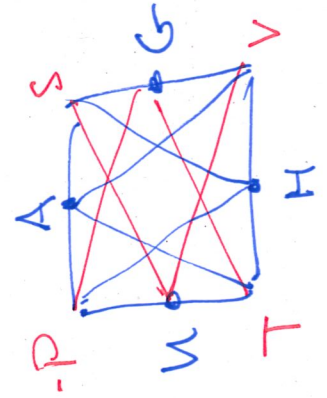
$$\begin{bmatrix} s \\ v \\ i \\ \vdots \\ u \end{bmatrix} \begin{bmatrix} T \\ \mu \end{bmatrix} = \begin{bmatrix} h \\ i \end{bmatrix} = \begin{bmatrix} u + Pv \end{bmatrix}$$

$$u = Ts + Pv + \mu N$$

$$h = Ts + \mu N \quad \Sigma = u - (-P)v$$



Bern Square?



Legendre Transform defines the natural variables of

the new function $\Sigma(\psi_1 \dots \psi_r, \psi_{r+1} \dots \psi_n)$

→ normal math one never differentiates a function with respect to anything other than a natural variable, e.g. $\partial U / \partial T = ?$

→ Thermodynamics all the time

$\frac{\partial U}{\partial S}$ unadorned means differentiating w/ ~~resp~~ natural variables held constant, i.e. $= \left(\frac{\partial U}{\partial S} \right)_{V,N}$

$\neq \left(\frac{\partial U}{\partial S} \right)_{P,N}$ if variables that are held cst are not natural variables then they must be indicated.

→ Theory $U(S,V)$ $dU = TdS + (-P)dV$
 $\Rightarrow T(S,V), -P(S,V)$

→ Practice $G(P,T)$ $dG = VdP + SdT$
 $\Rightarrow V(P,T), S(P,T)$

$$g = g_0 + c_0 T + c_1 P + c_2 P, T$$

$$s(P,T) = ?$$

$$v(P,T) = ?$$

Why bother with P.D. transformations? Knowledge of one function gives all functions.

Some examples:

= Problems 4.5-4.8 → to be assigned

Calorimetry - Problem 4.6

2021 8.3

est V (T) $\left(\frac{\partial T}{\partial q}\right)_V = \left(\frac{\partial q}{\partial T}\right)_V = \frac{1}{C_V}$

$du = dq - dws$
 $du_V = dq_V$

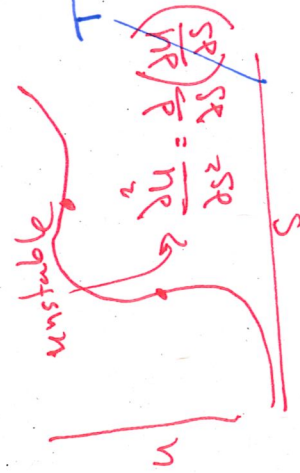
$C_V = \left(\frac{\partial u}{\partial T}\right)_V = \left(\frac{T \partial s - p \partial x}{\partial T}\right)_V$
 $= T \left(\frac{\partial s}{\partial T}\right)_V \Rightarrow S(T, V)$

est P (T) $\left(\frac{\partial T}{\partial q}\right)_P = \left(\frac{\partial q}{\partial T}\right)_P = \frac{1}{C_P}$

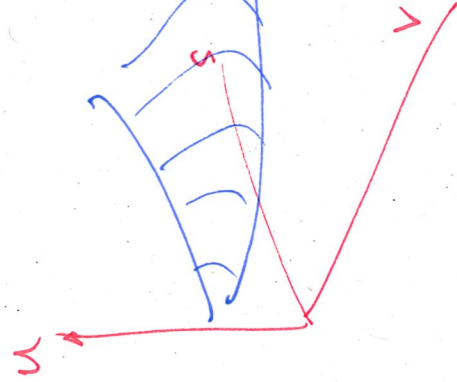
$dg = du + dw$
 $= du + p dv = dh$
 $dh = T ds + v dp$
 $C_P = \left(\frac{\partial h}{\partial T}\right)_P = \left(\frac{T \partial s + v \partial p}{\partial T}\right)_P$
 $= T \left(\frac{\partial s}{\partial T}\right)_P \Rightarrow S(T, P)$

Stability of a state of matter

Problem 4.8



$C_P - C_V = T \left(\left(\frac{\partial s}{\partial T} \right)_P - \left(\frac{\partial s}{\partial T} \right)_V \right)$
 $= \left(\frac{\partial T}{\partial s} \right)_V = \frac{1}{C_V} > 0$



$C = \begin{bmatrix} \frac{\partial^2 u}{\partial s^2} & \frac{\partial^2 u}{\partial s \partial v} \\ \frac{\partial^2 u}{\partial v \partial s} & \frac{\partial^2 u}{\partial v^2} \end{bmatrix} = \text{Det } C \geq 0$

$= \frac{1}{T} \left(\frac{\partial v}{\partial s} \right)_T - \left(\frac{\partial^2 u}{\partial v^2} \right)_s$
 $= \frac{1}{T} \left(\frac{\partial v}{\partial s} \right)_T \Rightarrow v(T, s)$

$|C| = \frac{1}{(V \frac{C_P}{K_T T} - V \kappa_T^2)}$

→ a state of matter is only stable if

$C_P / K_T > \kappa_T^2$

Problem 4.5 Seismic waves $\approx$ Elastic waves = Thermodynamic waves

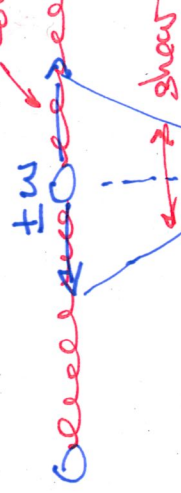
$$\text{Hooke's law} \Rightarrow F = k \Delta x$$

$$\text{Newton's law} \Rightarrow F = ma$$

$\vec{r} + w$

Compression $\rightarrow C_p \Rightarrow$ shear wave

compression



if no shear strength $C_p = C_p \text{ solid}$

$$C_{ID}^2 = \frac{\partial F}{\partial x} \times \rho_{ID} \quad \rho_{ID} = M/x$$

$$\frac{\Delta x}{x} = \text{strain}$$

$$C_{SD}^2 = -\frac{\partial P}{\partial V} / \rho_{SD} \quad \rho_{SD} = M/V$$

$$C_p = \sqrt{k/\rho} = \sqrt{\frac{F}{m}}$$

$$C_s = V_p^2 - \frac{4}{3} V_s^2$$

$$\frac{\Delta V}{V} = \text{bulk strain}$$

$$-\frac{\partial P}{\partial V} = K \rightarrow \text{bulk modulus}$$

$$\frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_P \Rightarrow V(P,T)$$

$$K_T = - \left(\frac{\partial P}{\partial V} \right)_T$$

$$K_S = - \left(\frac{\partial P}{\partial V} \right)_S$$

which is a better spring?

would you expect Quality to be frequency dependent?

differentiation rules in chapter 4:

x, y, z variables that can be used for differentiation (P, T)

S, g, z all the others (S, V)

$$\text{Rule 0 (4.39)} \quad 1 / \frac{\partial x}{\partial y} = \frac{\partial y}{\partial x} \Rightarrow \left(\frac{\partial T}{\partial V} \right)_P = 1 / \left(\frac{\partial V}{\partial T} \right)_P = 1 / \frac{\partial g}{\partial P}$$

$$\text{Rule 1 (4.43)} \quad \frac{\frac{\partial f}{\partial x}}{\frac{\partial y}{\partial x}} = \frac{\partial f}{\partial y} \Rightarrow \left(\frac{\partial S}{\partial V} \right)_T = \frac{\left(\frac{\partial S}{\partial P} \right)_T}{\left(\frac{\partial V}{\partial P} \right)_T}$$

Rule 3 Euler's criterion

$$\left(\frac{\partial y}{\partial x} \right)_z = - \left(\frac{\partial z}{\partial x} \right)_y / \left(\frac{\partial z}{\partial y} \right)_x$$

Rule 4 Euler's chain rule
(4.40)

↑ variable you can't handle

$$\text{Problem 4.7} \rightarrow \left(\frac{\partial P}{\partial T} \right)_S \rightarrow \left(\frac{\partial P}{\partial T} \right)_S \Rightarrow V(P, T) \Rightarrow$$

$$dV = \left(\frac{\partial V}{\partial P} \right)_T dP + \left(\frac{\partial V}{\partial T} \right)_P dT$$

at cst $V = 0$

$$\left(\frac{\partial V}{\partial P} \right)_T dT = - \left(\frac{\partial V}{\partial T} \right)_P dT$$

$$\left(\frac{\partial P}{\partial T} \right)_V = - \left(\frac{\partial V}{\partial T} \right)_P / \left(\frac{\partial V}{\partial P} \right)_T$$

Rule 5 (4.42) - two variables
you can't handle $\left(\frac{\partial S}{\partial T} \right)_V$

$$dS = \left(\frac{\partial S}{\partial P} \right)_T dP + \left(\frac{\partial S}{\partial T} \right)_P dT$$

$$\left(\frac{\partial S}{\partial T} \right)_V = \left(\frac{\partial S}{\partial P} \right)_T \left(\frac{\partial P}{\partial T} \right)_V + \left(\frac{\partial S}{\partial T} \right)_P \left(\frac{\partial T}{\partial T} \right)_V$$

Not Problem 4.4

$\rho = N / V$ ← molar mass at

V ← specific volume

4.5, 4.7

problem 4.7 g - gravitational acceleration at cst.

Make script $g(P, T)$

Maple script

```

g := G(P,T);  # makes g a symbolic f(P,T)
S := -d.f.f(g,T);  # makes S, V functions of P,T
V = d.f.f(g,P);  #

dsdpt := d.f.f(S,P);  - - - -
dpdpt := 1/dsdpt;  - - - -

```

Useful to have the solutions in Maple for

Chapter 5.